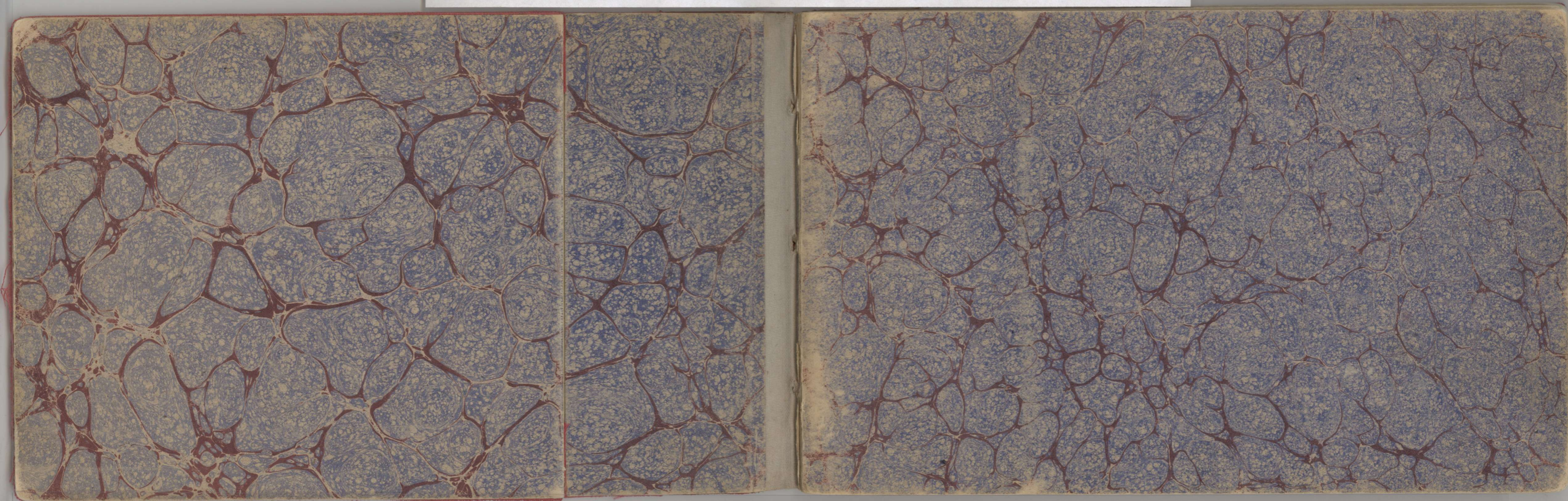


69

FIELDBOOK.
A.

H. A. DEPT.

Example of Marbled Endpapers



FIELD NOTES OF SURVEYS

from the 30th June to the 30th August 1910

Transmitted to the District Surveyor at Director of Surveys, Federal Capital Site

Pearce
N. S. W

with my letter dated

(Signature) P. L. Sheaffe
Surveyor
28-1-1910
St 5770

48592

EXTRACT FROM DEPARTMENTAL SURVEY REGULATIONS.

FIELD NOTES OF SURVEY.

Field-books supplied by the Department shall be used.
As a general rule one field-book should be completed before another is commenced. Notes shall be entered consecutively according to dates of surveys. Within six months after completion of the book the index shall be filled in, and the book forwarded to the District Surveyor under registered post, accompanied by a letter. The inside cover of book to be endorsed "Field-notes of Surveys made by me between the and the Transmitted to the District Surveyor at with my letter of the (To be signed)."
As the field-notes are the primary records of survey, are accepted as evidence in a Court of Law, and are for departmental reference, it is of importance that they should be precise and complete, indexed for purposes of ready reference, and kept in a neat and professional manner.
The diagram form of keeping field-notes is now generally adopted. Those Surveyors who have been accustomed to the old-fashioned form of record, and prefer it, should also provide a diagram in illustration. Field-notes should be so perspicuous that a qualified draftsman may be enabled to prepare plan therefrom without undue loss of time in investigation.
Field-books shall contain the notes actually taken in the field, not copies merely, and it is desirable that they shall be recorded in ink.
In the event of alteration of a mistake, there should be no erasure, but the erroneous entry should be neatly struck through, and the correction written above.
Date of survey, portion No., parish, county, applicant's name, and purpose of survey; registration Nos. (e.g., for conditional purchase, homestead lease, special lease, &c.), shall be first entered in each case; and the number and date of letter transmitting plan shall be added in due course.
The initial line of every survey, and azimuth adopted, shall be clearly indicated.
Bearings shall be clearly shown, with particulars of repetition of angles.
Lengths shall be entered as read, corrections for hypotenusal measurement and temperature shall be noted, and the lengths deduced therefrom shall be distinctly indicated.
Whenever there may be a close in the measurement of an area, or in a feature survey, or road survey, the closing angle shall be observed and noted.
References to corner trees may either be shown on diagram or in tabular form referred to in diagram by alphabetical letters.
Features shall be shown comprehensively, so that a draftsman may be enabled to represent the general aspect of the country.
On measured lines, the intersections of watercourses, summits of ranges, other natural features, fences, &c., &c., shall be correctly noted; lines reclaimed should be so specified. Position and state of preservation of old marks shall be carefully noted.
Intersections, offsets, and widths of watercourses shall be shown in the traverse of features. It is not sufficient to draw them without noting distances. The positions of improvements shall be clearly indicated; particulars of ownership, description, and value shall be entered, and also the dates when the improvements were effected.
Full particulars shall be stated as to the character of soil and timber, grazing or agricultural capabilities, and the geological formation of the country.
The Surveyor shall take such notes whilst in the field as will enable him in his letter transmitting the plan to report precisely in any case what natural boundaries or parts thereof might be exempted from the condition of fencing.
Notes shall be made of the estimated capital and rental values of land. These may be specially useful to the Surveyor when called upon to give evidence in Court. St 5770

INDEX.

Page	Particulars of Survey.	Date.
1	Observations at Coree A	30 - 6 - 1910
1 to 8 and 13 - 18	Survey of Boundary line Coree A to One Tree (part) (Sketch in pocket of book)	July and August 1910
8 - 10 21 - 23	Rechainage Boundary line from Wood N ^o 61 on Blue Range to Coree A	" " " "
25	Observations at One Tree A	July 1910

11-12 Check chainage was 100 to
wood 62

Note:- Line Coree A to One Tree A
Correct bearing is
54° 20' 19"
See papers 19th/468.

Station	Angle	Dist	Temp	Remarks
1	11° 30'	38	11	31.5
2	11° 35'	35	11	34.5
3	11° 34'	33	11	34.2
4	11° 31'	31	11	31.0
5	11° 28'	28	11	28.5
6	11° 26'	25	11	26.7
7	11° 24'	22	11	24.0
8	11° 22'	19	11	22.5
9	11° 20'	16	11	20.0
10	11° 18'	13	11	18.5

Slope	Chainage	Temp	Cor ^{tes} for slope, sag and chain	Corrected hor ^{tal} dist.	Remarks
6° 37'	063.13				On line Goree Trig to One Tree Trig from Goree Trig.
6° 37'	063.13				to observing st ⁿ
13° 02'	318.48				
12° 45'	503.77				
11° 36 1/4'	265.02				
					Wad ① tally
14° 46 1/4'	514.20				
11° 45'	455.40				Wad ② on crown of spur tally
7° 27'	506.98				
5° 31'	090.24				(with tape) to Wad ③ not on ropes, stony knobs 200 right
12° 0'	204.315				to Wad ④ not on ropes tally
	-27.02				to peg
12° 34'	500.45				
					Wad ⑤
17° 31 1/4'	202.38				Wad ⑤
17° 37'	486.09				Wad ⑥
0° 0'	010.97				Wad ⑥

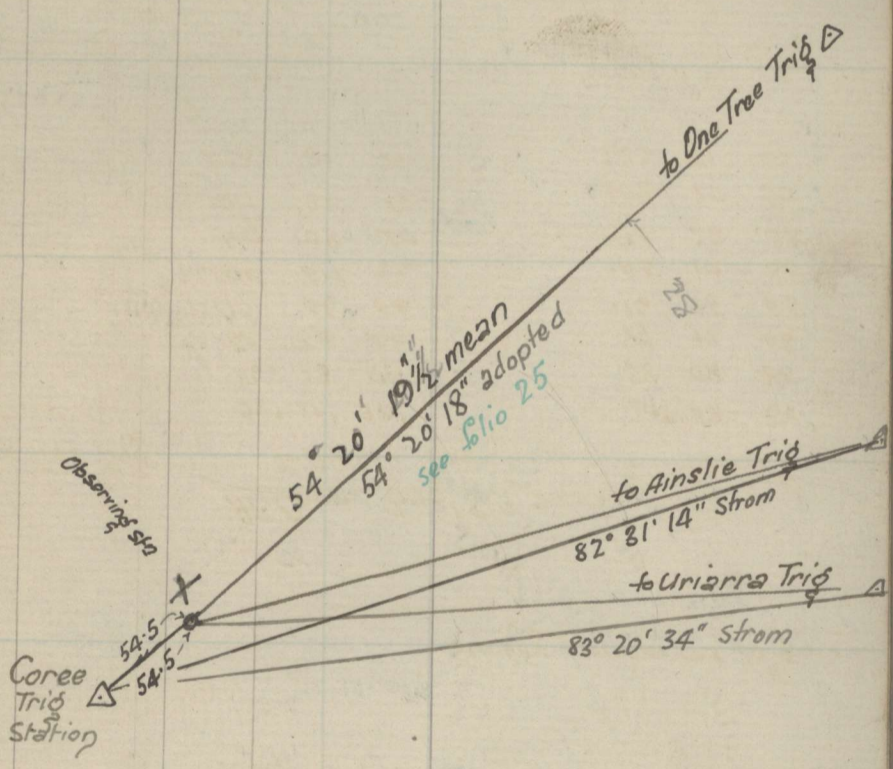
See next page

— Survey of part of boundary line —
of Commonwealth Territory and State
of N. S. Wales

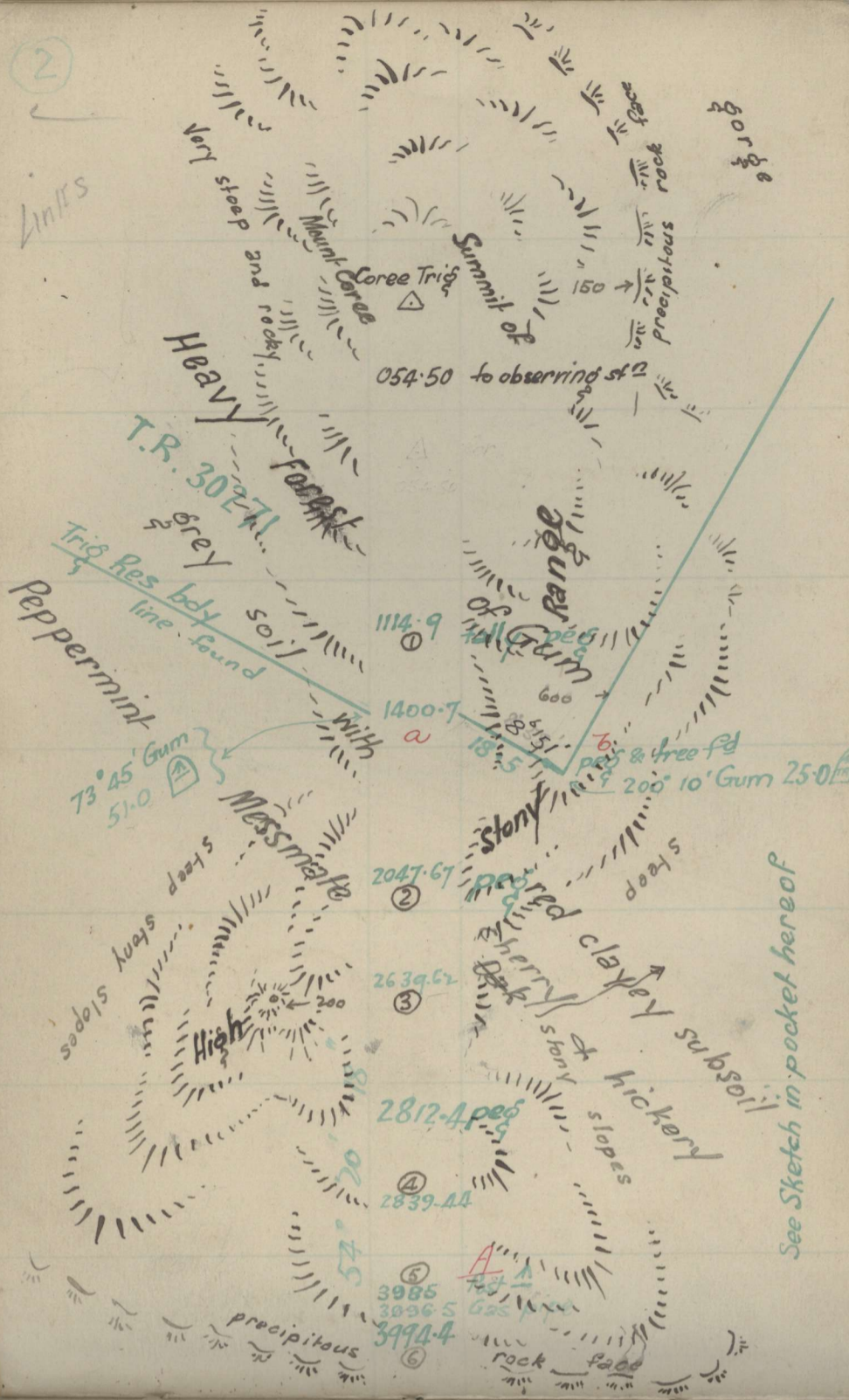
From Coree Trigonometrical Sta to One Tree Trig Trig Sta

Survey commenced 30th June '10

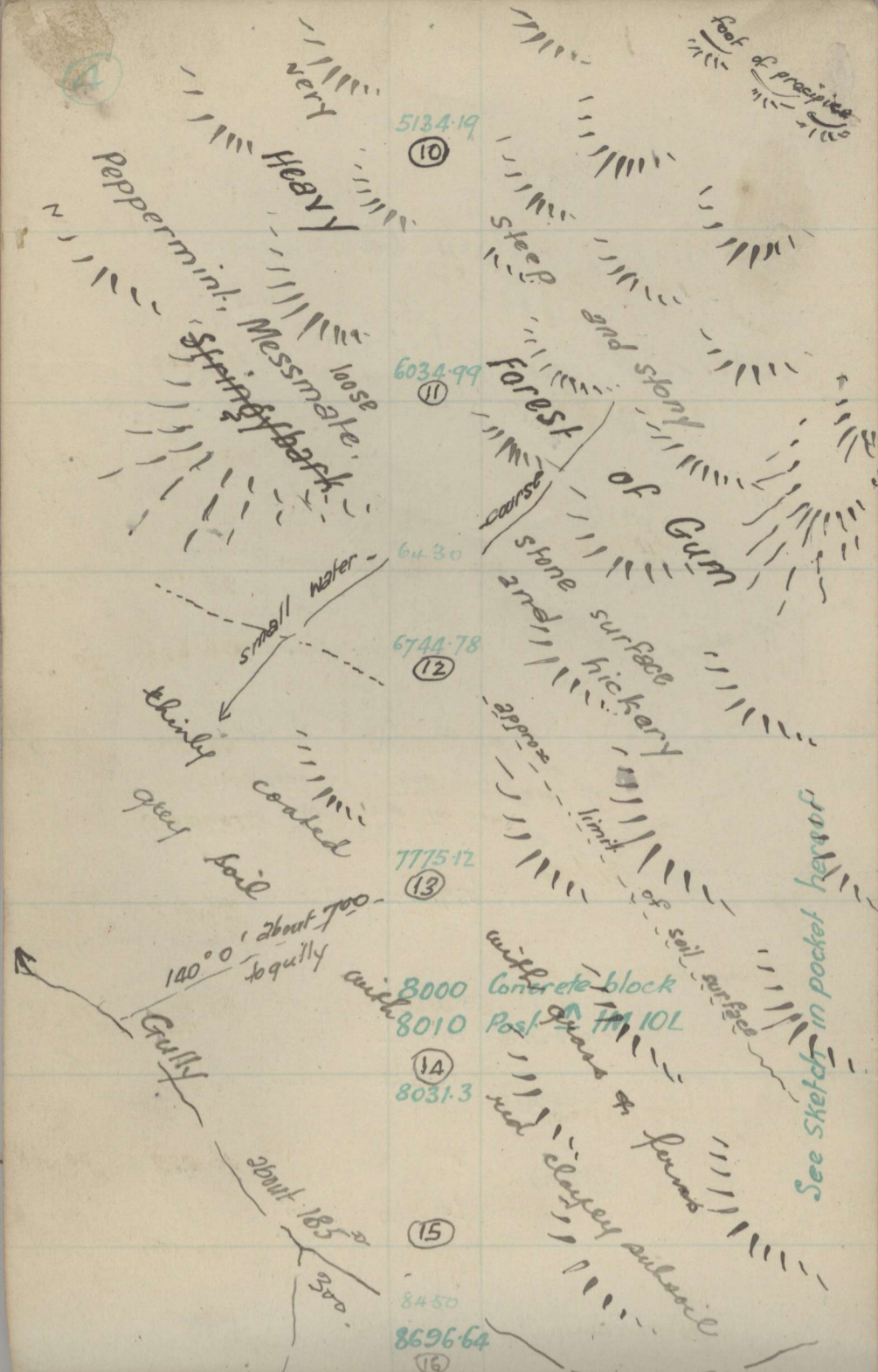
On One Tree Trig 360° 00' 00"	At <u>Coree Trig Sta</u> (approx) Sta X		mean angle 28° 11' 17" for reduction to Corey A	mean angle 29° 03' 58" for reduction to Corey A
	To Ainslie Trig	To Uriarra Trig		
	28° 11' 30"	29° 03' 50"		
	56 23 05	58 08 00		
	84 34 44	87 12 06		
	112 46 04	116 15 55		
	140 57 22	145 19 55		
	169 08 40	174 23 52		
	197 20 12	203 27 50		
	225 31 30	232 31 42		
Coree A-Ainslie A angle	82° 31' 14" 28 10 54	Coree A-Uriarra A angle	83° 20' 34" 29 00 17	
" A-One Tree A =	54° 20' 20" Strom 19.1	Coree A to One Tree A =	54° 20' 17" Strom	



(2)

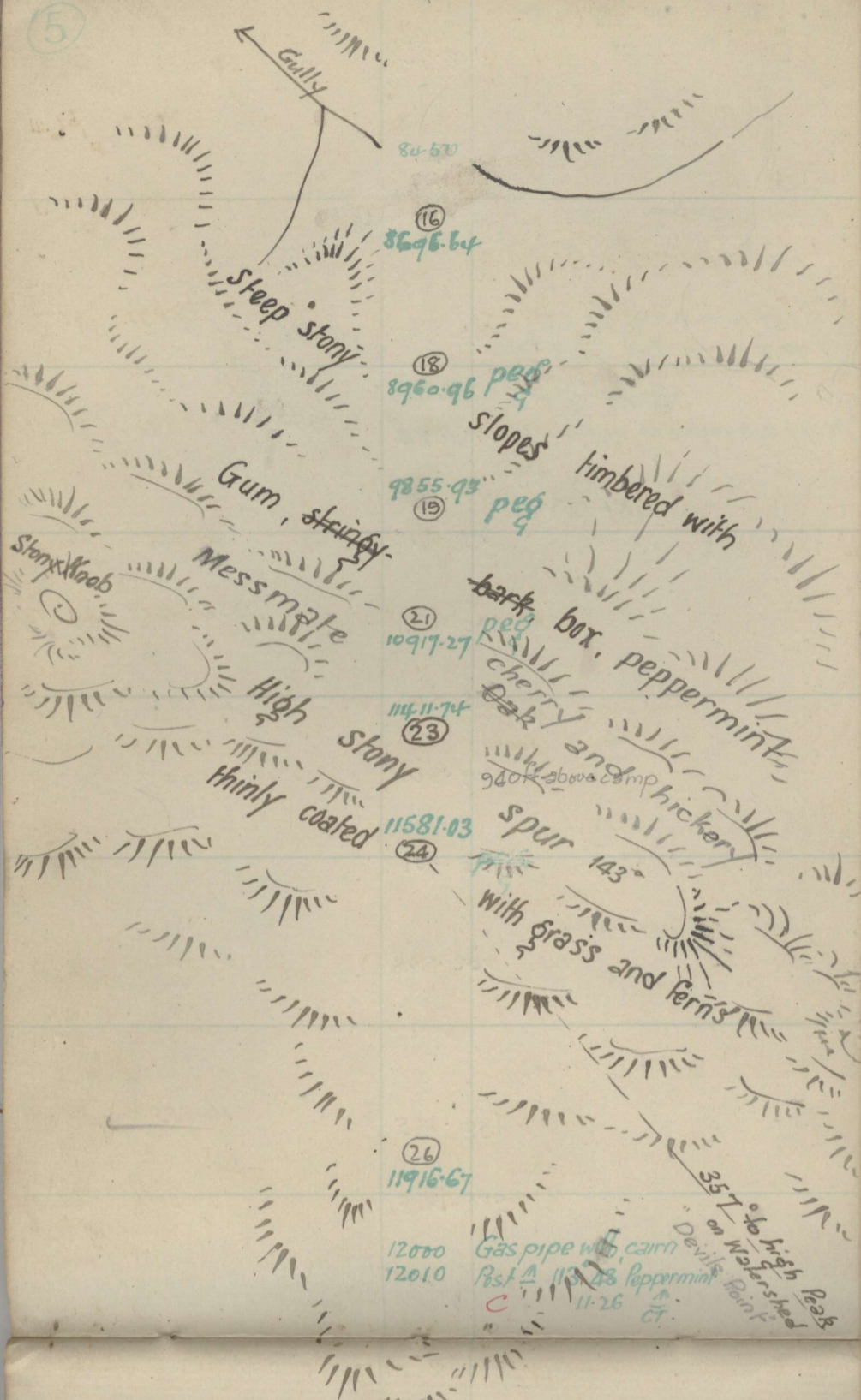


Slope	Chainage	Corrections Saf. slope chain	Correct- horizontal dist.	Remarks
0° 0'	054.50		054.50	From Coree Trig to Observing Sta
13° 02' d	318.48		310.208	
12° 55' d	503.77		490.486	
11° 36 1/2' d	265.02		259.490	to wad ① tally peg
14° 46 1/2' d	504.20		486.992	
11° 45' d	455.40		445.462	to wad ② on crown of spur. tally
7° 27' d	506.98		502.128	
5° 31' d	090.24		089.845	(with tape) to wad ③ stony knob 200 to right
12° 0' d	204.315		199.84	to wad ④ -27.20 to tally peg
12° 34' d	500.45		487.903	to wad ⑤
17° 31 1/2' d	202.38		192.98	
17° 37' d	486.09		462.84	3996.5 At 3985 Gas pipe with cairn At 3996.5 post (3985.0) 33° 37' Gum 20-13 142° 45' Gum 53-27
0° 0'	010.97		10.97	to wad ⑥ peg 39° 58' (16° 56' 30-48) Gum 132° 45' (8° 42' 54-82)

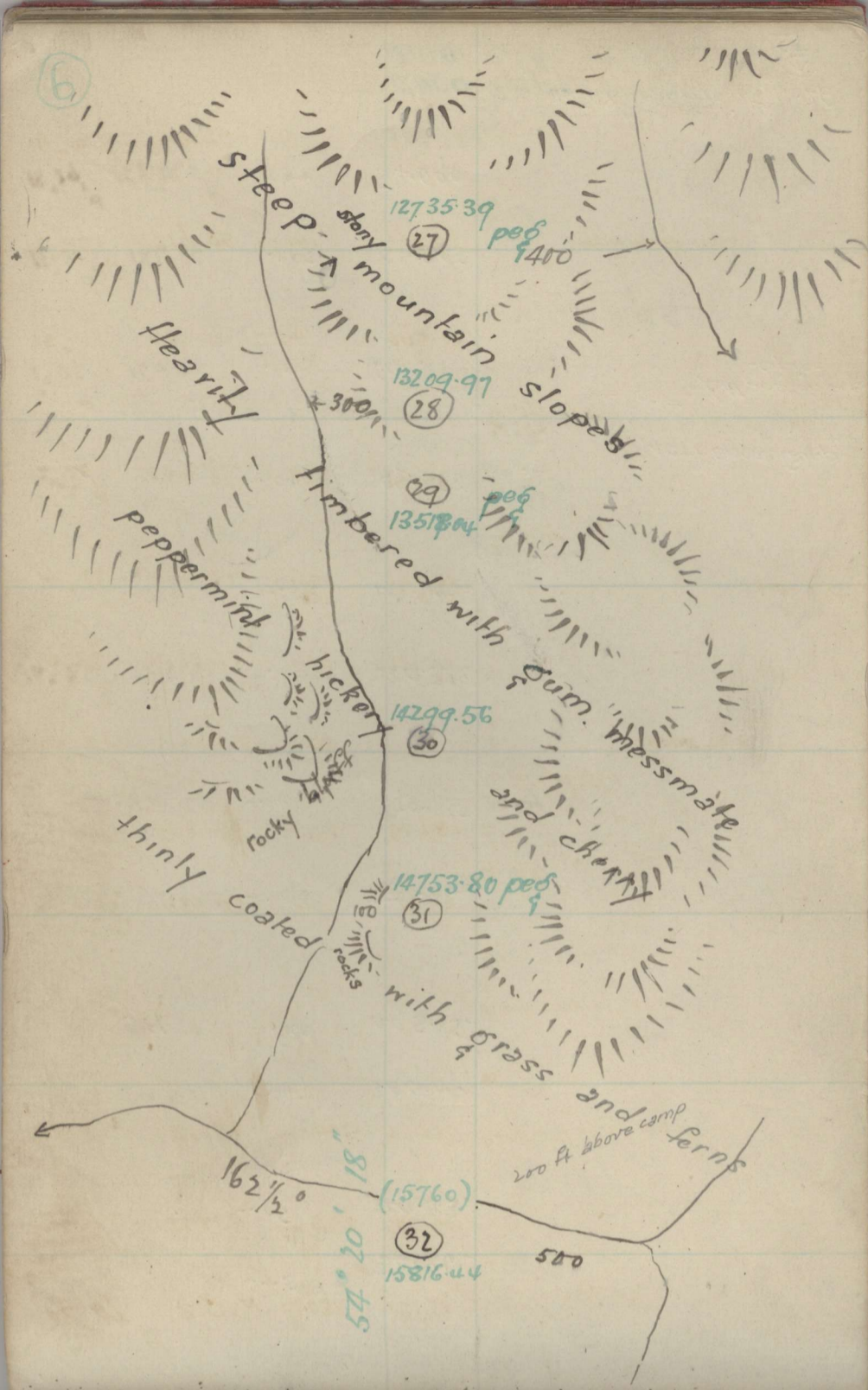


21° 37' ^d	408.58		379.345	from wad (10)
19° 35' ^d	553.91		521.367	wad (11) tally ✓
9° 30' ^d	376 307.615		303.294	+ 100 to head small gully
7° 55' ^d	410.74 ²⁵		406.525	tally (12) ✓
7° 14' ^d	500.21		495.622	
6° 27' ^d	305.37		303.328	
5° 58' ^d	129.955		129.256	
1° 40' ^d	101.86		101.527	to (13) tally
1° 58' ^d	256.34	256.18	8000	Iron spike in concrete block
			8010	Post IM 10L
9° 40' ^d	272.39	268.50	B	to (14) peg for chain, but not aligned
				{ 18° 56' Peppermint 41.45 (A)
				{ 139° 25' Peppermint 45.2 (C.T.)
				to (15) peg, but not aligned
				+ 150 to gully, flooring 185°
2° 15' ^e	397.42		396.824	to (16) tally peg

(5)



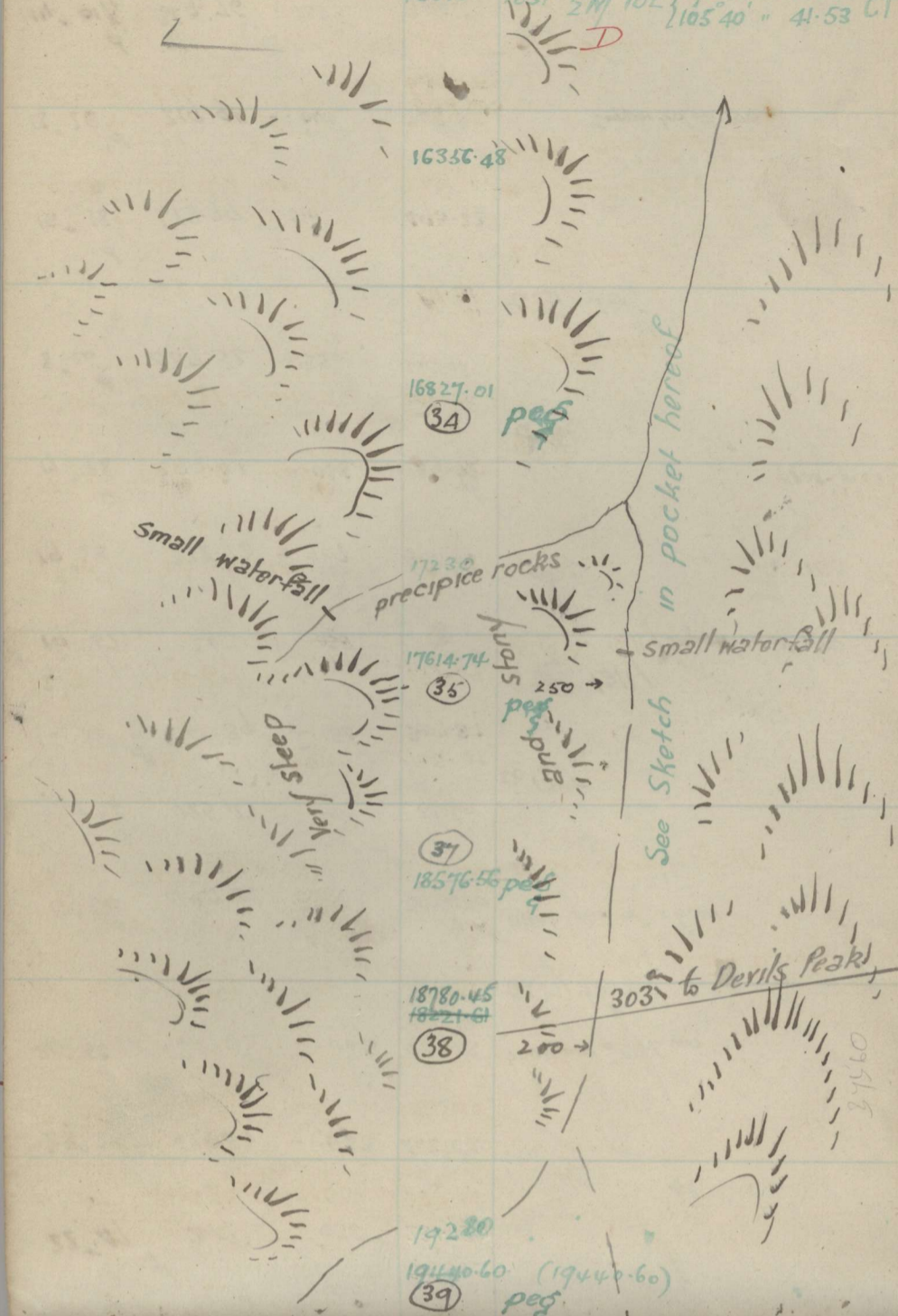
7° 45'	136.15	-05	134.862	to (17)
3° 37'	129.69	-05	129.437	to (18) tally
9° 55'	405.44	-347	399.087	
14° 0'	511.68	-680	495.852	to (19) tally
19° 25 1/2'	563.75	-674	531.062	
20° 38'	310.65	-148	290.745 (no sag)	1061.15 to (20)
15° 28'	248.32	-043	239.358	no sag to (21) tally
11° 10'	215.72	-043	211.617	to (22) peg
7° 4'	285.00	-043	282.868	no sag to (23) peg + 050 to top of spur 143° 6° 05' to full position precipice
1° 23'	169.35	-	169.30	no sag to (24) tally High Peak 357'
13° 27'	186.66	-005	181.545	to (25)
18° 29'	162.465	-004	154.090	(+83.33) to (26)
			12000. Gas pipe with cairn	11-26
			12010. Post A, 113° 48' Peppermint	11-26



$22^\circ 47'$	251.41	$-.038$	231.780	
$23^\circ 25'$	504.69	$-.563$	462.641	
$20^\circ 58'$	132.62	$-.005$	123.833	back end of chain to (27) tally
$13^\circ 54'$	404.22	$-.316$	392.109	back end of chain
$14^\circ 33'$	085.43	$-.01$	82.69	to (28)
$15^\circ 21'$	319.39	$-.134$	307.89	to (29) tally
$19^\circ 52\frac{1}{2}'$	202.29	$-.009$ $-.038$	190.25	supported at 100
$19^\circ 28'$	332.72	$-.050$ $-.029$	313.76	" " 160
$17^\circ 28'$	290.42	$-.131$ $-.038$	277.82	(300-9.58) to (30)
$8^\circ 20'$	459.32	$-.333$	454.18	to (31) tally
$15^\circ 18'$	513.99	$-.610$	495.22	
$18^\circ 26'$	219.95	$-.01$ $-.041$	208.67	- supported at 100
$14^\circ 01\frac{1}{2}'$	369.76	$-.135$	358.63	to (32) tally - 050 to quarry bearing $162\frac{1}{2}^\circ$

7

16000 Iron spike in concrete block
 16010 Post 2M 10L 195° 30' Gum 16.26 ↑
 105° 40' 41.53 GT



(+183.56)

16000 Iron spike in concrete block with ^{cap}

16010 Post 2M 10L 195° 30' Gum 16.26 ↑
 389.56 105° 40' Gum 41.53 GT

14° 37' 4 202.895 - .346

12° 45' 154.27 - .005

14° 15' 485.81 - .346

13° 12' 539.98 - .680

38° 40' 135.00 - .009

18° 18' 165.67 - .005

9° 10' 529.08 - .681

18° 70' 089.66 - .005

16° 44' 309.21 - .144

17° 17' 062.22 - .005

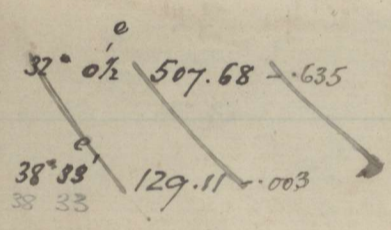
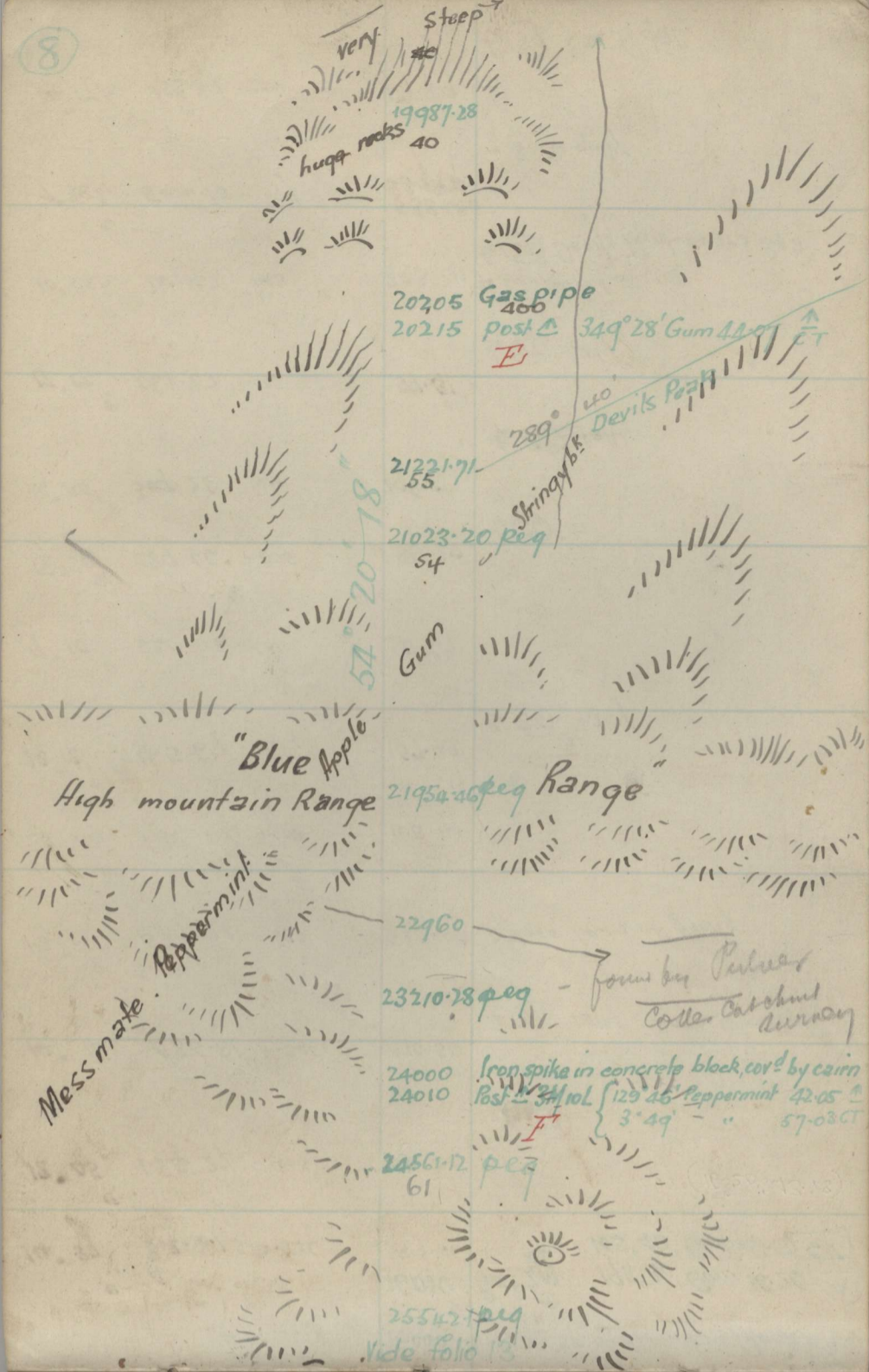
10° 54 1/2 207.65 - .043

7° 38 1/4 544.15 - .679

24° 17 1/2 133.29 - .004

150.47 (16° 20' 43.28)
 to 33
 to 34 tally. +400 to gully
 525.09 across head of gully
 105.41
 157.29 to 35 tally
 521.69
 85.20 to 36
 296.00 to 37 tally
 59.81 to 37 tally
 203.91 supported at 100 to 38 Devils Point bears 303°
 538.685
 539.16 - 30 to gully
 121.49
 to 39 tally

109



to 40
 to 40 mark destroyed
 20205
 20215 post Δ 349° 28' Gum 44.07 Δ CT

From post 2610		1000 ft. state camp
0° 0'	049.35	049.35
10° 31 1/2	419.44 - .250	40° 412.865
21° 42'	373.415 - .100	40° 346.79
		to 54
22° 12'	214.48 - .03	40° 198.51
		to 55 Range 250° Devils Pk 287.40
19° 57 1/2	271.04 - .03	40° 254.49
		to 56
13° 55 1/2	297.52 - .012	40° 288.76
		sup ^{td} at 142 cl
		to 59
2° 52'	189.585 - .004	40° 189.32
		to tally peg 21954.465
6° 39'	258.995 - .03	38° 257.19
		Sup ^{td} at 2 cl
9° 55 1/2	372.965 - .035	38° 367.30
		Sup ^{td} at 2 cl
5° 5 3/4	388.945 - .485	38° 586.13 + 45.18 to peg = 23210.28
		+ 4° 03' 46.29 to tally

23210.28
 21954.46
 1255.82

11° 46 1/2 ^e	154.89	-.004	38°	151.12	
7° 07 1/8 ^e	308.48	-.105	38°	300.93	to 59 23617.14
7° 0' ^e	254.60	-.030	44°	252.64	
6° 52 1/8 ^e	317.55	-.035	44°	315.195	Sup'd at 200 ch ²
4° 38 1/2 ^e	380.475	-.036	42°	379.14	to 60 -9° 36 1/2 187.59 " " 2 ch ²
6° 47 3/4 ^d	165.135	-.005	42°	163.96	to 61
13° 19' ^d	387.13	-.06	42°	376.60	Sup'd at 400 400 -12.87

Vide fol. 13

From top ^{Blue} ~~Blanca~~ Range, back towards Coree

From wad 61 folio 8

5° 59' ^d	182.52	-.006	181.525	3 rd
4° 6' ^d	198.19	-.043 -.006	197.66	200-1.81
7° 53 1/2 ^d	318.34	-.142	315.21	to 60
8° 22' ^d	255.74	-.043	252.60	to 59 tally 23617.14
8° 11' ^d	304.03	-.142	300.815	
2° 39' ^d	533.46	-.667	532.26	
9° 30' ^e	207.94	-.02 -.042	205.09	-180 to gully bearing 330° (sag on 150)
9° 10' ^e	372.155	-.040 -.139	367.39	to 58 tally 243 Supported at 150
5° 30' ^e	260.155	-.043	258.93	+ 50 to top of Range. 2° 38 1/2 elevation to Coree
4° 44 1/2 ^d	188.17	-.005	187. 178.526	to 57 tally
14° 51 1/2 ^d	298.73	-.132 -.040 -.015	288.745 297.71	(300 - 1.27) Supported at 142 chs (sight on Precipice wants to go 0.15)
21° 06 1/2 ^d	272.99	-.04	254.65	to 56. peg moved 0.1 South
				to 55

23° 28' ^d 216.435 - .037 198.52

to 54 tally

22° 23' ^d 375.125 - .126 346.78

to 53

10° 58 1/3 ^d 468.825 - .325 459.98

6° 50' ^d 033.70 33.46

to 52 ⁴¹ road on trial 2.11 N tally

30° 19' ^d 225.87 - .034 194.97

0° 0' 0.71 .71

to 40 see Folio 21

From Wad 100 page 16

From 100

e	4° 0 1/2	268.715	-.01	48°	268.04	Sup ^d at 100
e	8° 27 3/4	504.23	-.49	48°	498.235	+250 to gully. flowing 99° 947.71
e	20° 04'	193.21	-.03	50°	181.45	to 99
e	18° 50'	368.945	-.035	50°	349.151	to 98 sup ^d at 100
e	15° 22 1/4	163.36	-.01	50°	157.504	to 97
e	7° 51 1/2	164.67	-.01	50°	163.11	to 96
o° 0'		021.07		3	021.07	to 96
d	11° 43'	141.08	-.01	52°	138.125	to 96
d	22° 24 1/4	173.26	-.01	52°	160.19	
d	27° 41'	126.55	-.006	53°	112.06	to 95 near fence + 050 to gully
e	14° 05'	407.32	-.247	53°	394.838	to 94
e	13° 48 2/3	264.74	-.015	54°	257.072	Sup ^d at 100 to 93
e	5° 04'	286.235	.015	54°	285.086	sup ^d at 100
o° 0'		075.89			075.84	to 92
e	6° 49 1/2	529.08	-.49	54°	524.77	to 91
e	11° 56'	236.475	-.01	53°	231.345	Sup ^d at 100 to 90
e	11° 55 1/4	531.15	-.14	52°	519.50	to 89 sup ^d at 200
e	13° 35 1/4	426.33	-.04	52°	414.32	to 88 sup ^d at 300 + 300
o° 0'		014.01			014.01	+ 200 to gully flowing 80°
e	22° 22 1/3	500.42	- 480	53°	462.26	
e From here on -- 19 from all distances for broken chain						
e	29° 24 1/2	176.855	-.025	52°	153.88	to 87
e	24° 23'	359.03	-.025	51°	326.785	to 86 sup ^d at 100
e	19° 24 1/3	197.665	-.03	51°	186.32	to 85 31853.810
e	11° 31 3/4	185.95	-.020	50°	181.99	to 84 trial line .16 too far south 31667.580
e	12° 32 1/4	580.83	-.490	50°	566.23	to 83
o° 0'		029.38			029.19	to 83 31485.600
e	7° 11'	126.67	-.01	49°	125.48	
o° 16'		236.85	-.01	49°	236.63	sup ^d 100 to 82 30528.070
d	3° 56 1/2	532.45	-.14	48°	530.78	sup ^d at 300 32.45
e	5° 40 3/4	543.875	-.14	48°	540.807	to 81 head small gully 29977.260 sup ^d at 300
						to 80 29456.939 (+.04 to page)

^e
4° 0 1/2 406.16 - .06 48° 404.865 sup^{td} at 200
to 79

^d
1° 58' 116.57 - .006 48° 116.30 to 79 28935.287
+180 to gully flowing 144°

^e
6° 40' 500.80 - .488 48° 496.67

^e
11° 52 1/3 125.96 .01 46° 123.09
to 78

^e
6° 52 3/4 094.14 093.27 to 78 28222.287 (+.02 per)

^d
2° 09' 234.00 .01 46° 233.62 sup^{td} at 100

^d
9° 38' 205.965 - .01 46° 202.845 sup^{td} at 100
to 77 27785.829

^e
12° 45 1/2 560.38 - .255 45° 546.04 + 100 to gully
sup^{td} at 100
to 76 27239.767

^e
5° 04' 263.805 - .03 45° 262.51 + 200 to gully

^e
16° 50 1/4 445.98 - .250 45° 426.48 to 65 26550.809

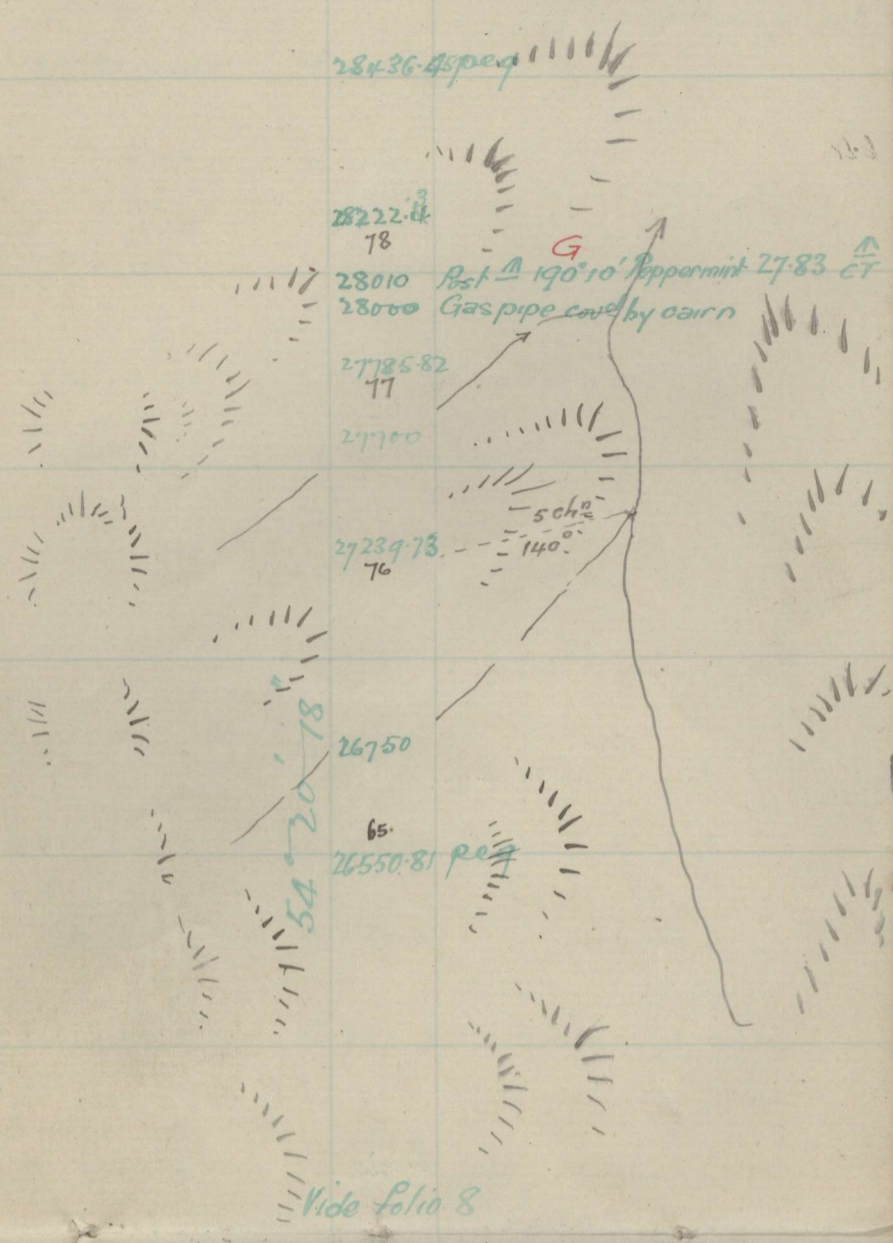
^e
20° 02 1/4 512.71 - .13 44° 481.30 sup^{td} at 200

^e
22° 50' 569.65 - .127 44° 520.99 " " 300

^e
14° 39 1/2 369.54 - .035 45° 357.205 to 64 25548.552
516 23

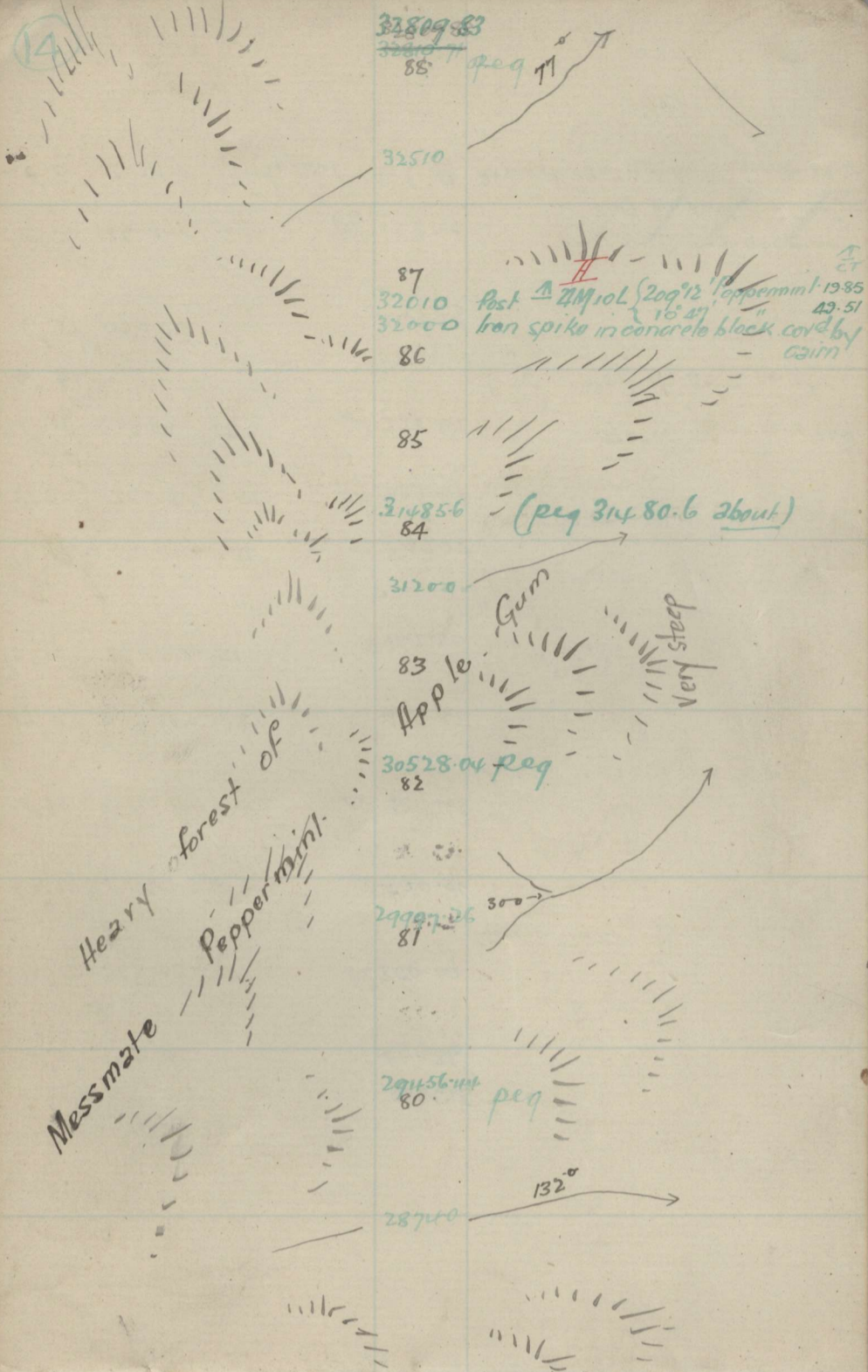
^e
12° 43 1/2 089.0 45° 086.825 to 63 25104.69

^e
12° 23 1/4 385.855 - .04 47° 376.60 sup^{td} at 200
to 62



From Mad 63		
12° 43 1/2' 089.0	086.625	
0° 0' 007.36	007.36	
	-20	
d		
15° 10' 363.05 - 10	48 350.09	
d		
23° 19 3/4' 567.82 - 223	48 520.96	to 62 tally - 6.46 to peak sup ^{td} at 100
d		
20° 35 1/6' 514.47 - 125	48 481.265	" " 200 to 65 tally + 200 to gully
d		
17° 23' 447.28 - 287	48 426.42	
d		
6° 16 2/3' 264.30 - 01	48 262.50	sup ^{td} at 100 to 76
d		
13° 17 1/4' 561.84 - 46	48 548.09	
e		
8° 31 1/2' 205.315 - 01	47 202.83	to 77 peak - 100 to gully sup ^{td} at 100
e		
1° 06' 233.89 - 03	47 233.61	190° 16' Peppermint 27.83
d		
6° 51'		to 78 - 0° 49' 212.43 to post
d		
6° 51' 094.13	093.27	
d		
13° 53' 126.975 - 005	46 123.07	- 12.19 to post gas pipe - 2.19 to post
- 0° 0' 2.19	topost - 2.19	at post 130° 34' Peppermint 28.35 slope 10° 05'

[Handwritten signature]



32809-83
88

32510

87
32010
32000
86

Post Δ 4M 10L (209'12" Peppermint 1985
15'41" 49.51
Iron spike in concrete block covered by
grass

85
314856
84

(peg 314 80.6 about)

31200

83
Apple
30528.04
82

Gum
Very steep

Heavy forest of
Peppermint
Messmate

29997.26
81

29156.11
80

peg

28740

132°

From post Δ 28436.5

7° 03 1/3	503.375 - .47	47 498.84	300 to gully
0° 12'	116.51 - .005	47 116.31	to 99
4° 38'	406.46 - .06	47 404.83	sup'd at 200 to 80 peg
6° 08 1/2	544.29 - .065	47 540.835	sup'd at 100 + 300 to 81
3° 27 1/4	532.12 - .113	47 530.78	sup'd at 100 + 200 to 82 tally
1° 23'	236.925 - .01	47 236.635	" " 100
9° 19'	156.97 - .0	47 154.7 1/2	no sag
12° 54 1/2	581.64 - .468	47 566.245	+ 300 to head gully
12° 51 1/2	186.87 - .01	47 181.98	to 84
20° 37 1/4	199.215 - .01	47 186.24	to 85
+ 0° 0'	146.19 to 4M 10L		to 86

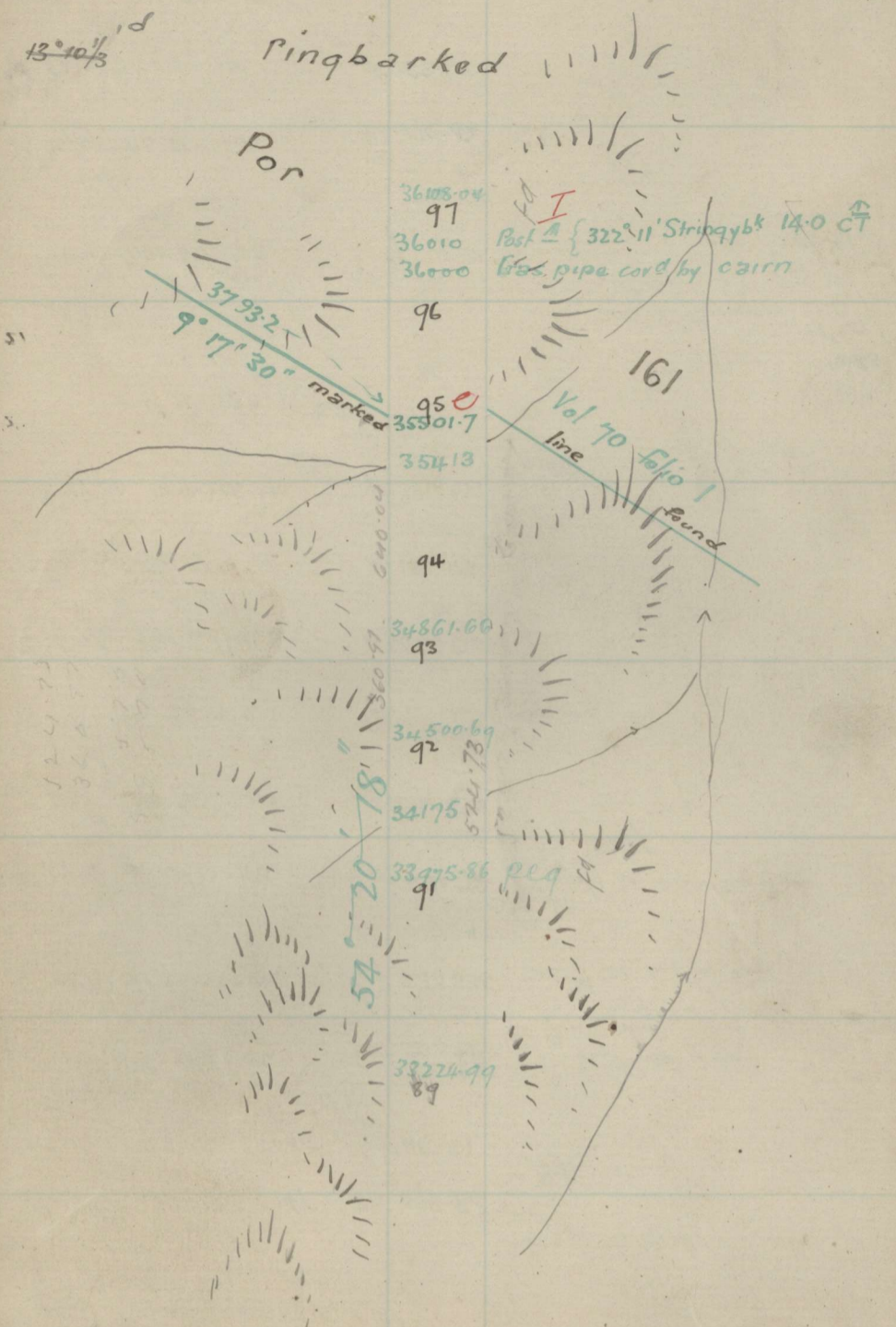
From Post 4M 10L

26° 26 1/3	190.51 - .01	48 170.42	to 87
30° 52 1/2	179.49 - .01	48 153.87	
22° 20'	515.52 - .423	48 476.275	

to 88 peg - 300 to gully

19-85
209'12" Peppermint { 19° 59' CT }
10° 47' " { 18° 34' }
52.23
49.51

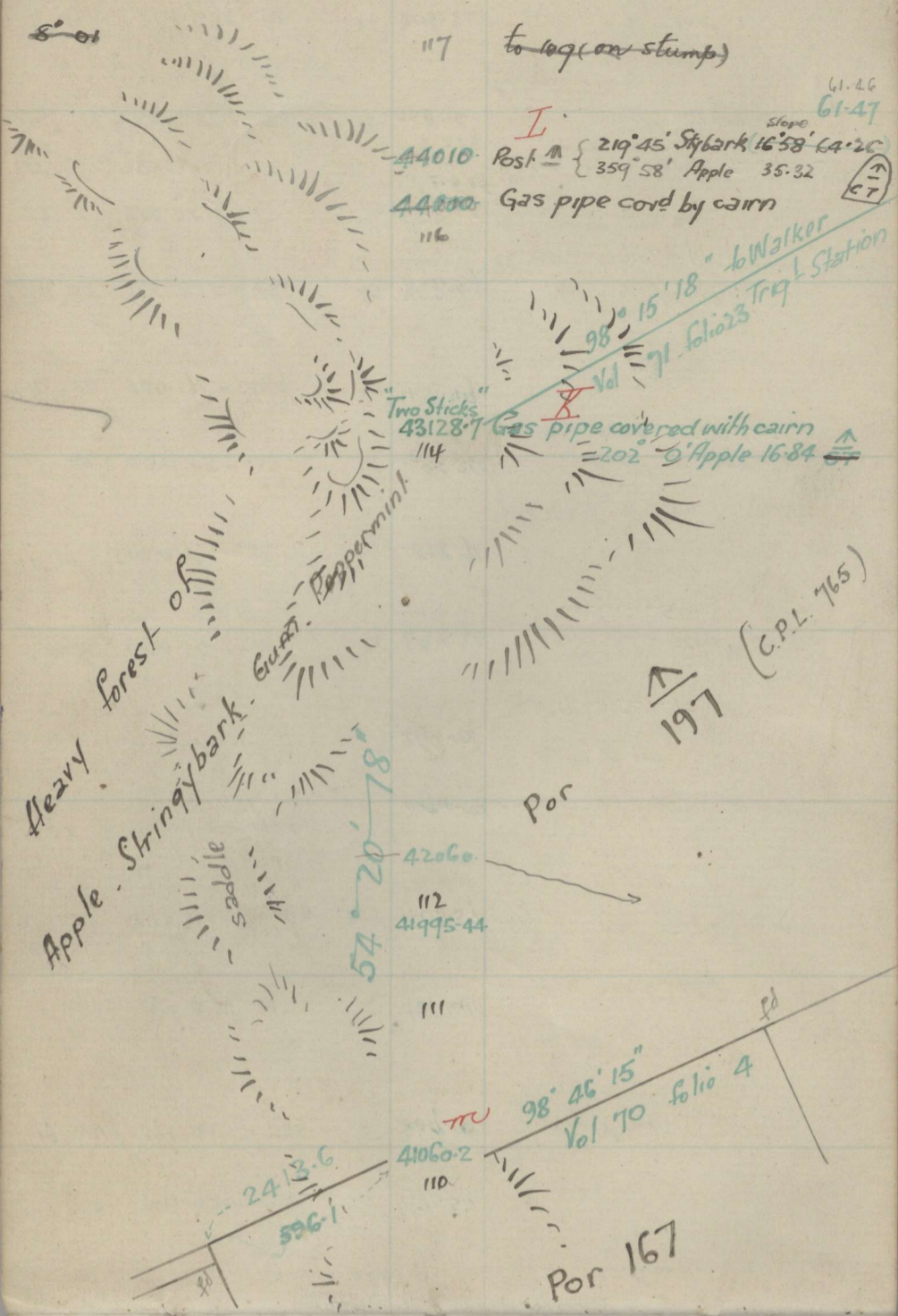
B



All distances 19 too great owing to broken chain

13° 10 1/3	358.28	-035	50°	348.63	sup ^d at 100
12° 20 1/4					
15° 53 1/2	068.44			065.64	to 89
12° 20 3/4	532.15	-132	50°	519.514	to 90 sup ^d at 200
12° 55'	237.60	-01	52°	231.39	" " 100
7° 19 3/4	529.84	-47	52°	524.85	to 91 pag + 200 to gully
0° 36'	105.21	-005		105.01	to 92
6° 04 1/3	257.64	-01	52°	255.99	to 93 sup ^d at 100
14° 45 1/2	266.08	-01	50°	257.106	" " 100
14° 40'	408.50	-234	50°	394.77	to 94
25° 50 1/2	124.72	-005	50°	112.09	to 95 -100 to gully -11.8 to bdy per 161
21° 00 1/3	171.795	-007	51°	160.18	to 96
9° 32 1/4	140.26	-006	51°	138.125	to 96 + 76.13 322' 11' Strip 14.0 CT
9° 38'	157.925	-006	52°	155.50	to 96 pag 8.47 78.45
9° 37'	029.26		28.66	89	to 97 36108.0145

[Handwritten signature]



-19 off all chainages for broken tape

8° 01'	133.48	- .005	65°	131.98	to 109 (on stump)
13 14 1/2	047.68			046.227	+ 28.75 to peg 157° 07' Stringbark (9° 03' 51.25)
19° 37 2/3	205.945	- .01	64°	193.80	to 110 near fence + 13° 24' 51.34 body (41056.46) + 2.5' = 41058.96 to body sup'd at 100
22° 28 3/4	553.98	- .133	67°	511.62	to 111 sup'd at 200
15° 31 1/4	242.685	- .01	60°	233.64	to 112 peg + 60 to head gully 41995.46 sup'd at 100
14° 35 1/4	336.07	- .035	58°	325.024	to 113 " " 200
18° 38 3/4	593.71	- .136	56°	563.72	
10° 26 3/4	155.925	- .01	56°	153.14	
4° 42 3/4	092.18			091.675	to 114 peg (43129.5v) 43128.7v Two Sticks
14° 11'	152.745	- .006	56°	147.90	
0° 0'	001.33			001.33	to 115
21° 36'	78.70			073.00	
23° 42 1/2	555.155	- .120	56°	508.02	sup'd at 200 to 116 peg (43257.85v) 142.247
20° 26 1/2	509.395	- .125	54°	477.08	" " 200 to 116
16° 33'	191.345	- .03	54°	183.23	to 117

197 (C.P.L. 765)

At Stony Ridge or "Pleasant" see Vol 71 fol 6

69072.8 from Coree Δ

On One Tree	On Pine Ridge	On Ranger
360° 0' 0"	45° 7' 42"	85° 13' 00"
359.59.58	45. 7. 42	85. 13. 00
Tel. Rev'd		
00. 00. 00	45. 7. 40	85. 13. 4
360. 00. 00	45. 7. 34	85. 13. 5
360. 00. 02		
90° 00' 00"	135° 7' 30"	175° 12' 44"
90. 00. 00	135. 7. 30	175. 12. 46
90. 00. 05		
Tel. Rev'd		
270		
89. 59. 58	315. 7. 35	355. 12. 46
270. 00. 00	315. 7. 25	355. 12. 37

Mean Angle 45° 07' 35 1/2"

40° 05' 19 1/2"

"Pleasant" to One Tree Δ 54 20 18" Strom
 " Pine Ridge Δ 99. 27' 53" Strom

On Walker	On Coree line	On Surveyor Hill
98° 12' 00"	179° 59' 56"	337° 45' 7"
98. 12. 00	179. 59. 55	337. 44. 50
98. 11. 56	180. 00. 00	337. 44. 48
98. 12. 00	180. 00. 00	337. 45. 00
188° 11' 48"	269° 59' 50"	247° 45' 00"
188. 11. 48	269. 59. 56	247. 44. 54
8. 11. 52	89. 59. 52	67. 44. 55
8. 11. 42	89. 59. 48	67. 44. 58
12° 59' 02 1/2"	81° 48' 03"	157° 44' 58 1/2"
06 1/2	01 1/2	50

Surveyor's Hill and One Tree
 angle 22° 15' 01 1/2"
 Pleasant-One Tree 54 20 18
 " - Surveyor 32° 05' 12" Strom

At Phillips. near Fairlyte Road
 54945.2 from Coree Δ

On One Tree	On Walker	Vol 71 folio 2
360° 6' 00"	63° 26' 22"	
	126 52 47	
	190 19 15	
	253 45 32	
	317 11 52	
	20 38 04	
	84 04 38	
	147 30 55	

Mean = 63° 26' 22"

Mean = 63° 26' 22"

54 20 18 Phillips to One Tree Δ
 117° 46' 40" " " Walker Δ

From post at 2012010

d.
23° 23 1/4 211.57 - .030 47° 194.13

d
23° 20 1/4 443.64 - .130 47° 407.18 sup^{td} at 300

d
21° 0 2/3 132.95 - .01 47° 124.09 - .20 to (27)
from 30

8° 22' 459.30 - 11 48° 454.24 sup^{td} at 100
to 31

From 29

19° 48' 202.90 190.88 sup^{td} at 100

From 36

d
17° 14 2/3 371.77 - .101 45° 354.91 to 37 back end of chain

e
7° 38 1/4 544.03 - .488 45° 538.64

e,
24° 13 1/2 133.26 - .005 45° 121.51 to 39

e
28° 29' 153.735 - .005 45° 135.16

34° 50 1/4 502.61 - .223 45° 412.28 sup^{td} at 100
(.71 to wad 40)

(2)
5° 01' 164.63 - .005 42° 163.97 to 61

Re-chaining of Bdy line from
wad 41 to Cove. Trig stn

Continued from folio 10

From 41

29° 11' 1/3 ^e	224.205	-.04	195.69 ^{.70}	to 40
35° 3' 23' 40" ^d	505.275	-.495	411.49	} 546.68 2 nd chain
29° 50' 30" ^d	155.80	-.004	135.14	
25° 47' ^d	134.88	-.005	121.455	
8° 7' 1/4 ^d	544.61	-.646 -.648	538.54	to 38
12° 18' ^d	208.65	-.01	203.89	supported at 100 to 37
17° 16' ^d	371.83	-.132	354.97	← 354.95 to 36
20° 45' 1/3 ^d	091.10		85.19	
9° 45' ^d	529.90	-.647	521.65	to 35
19° 38' ^d	166.99	-.005	157.29	

39° 40' 1/2 ^d	136.915	-.004	105.39	from here steel chain
13° 33' ^d	507.58	-.455	45° 525.01	to 34
15° 54' 2/3 ^d	258.81	-.455 -.031	45° 248.85	
14° 9' ^d	228.65	-.031	45° 221.66	to 33
14° 2' ^d	155.08	-.004	46° 150.43	
15° 10' ^d	403.97	-.233	46° 389.62	to 32
13° 22' ^e	368.76	-.106	46° 358.63	
17° 15' ^e	218.525	-.008 -.009	46° 208.67	supported at 100
14° 43' 1/3 ^e	512.74	-.489	46° 495.36	to 31
7° 48' 1/2 ^e	458.73	-.250	46° 454.26	to 30
16° 34' 2/3 ^e	289.08	-.03	46° 277.01	
18° 43' 3/4 ^e	331.44	-.103	46° 313.76	to 29
18° 44' 1/2 ^e	201.595	-.007	46° 190.88	supported at 100 to 29
14° 38' 1/3 ^e	318.36	-.034	46° 307.96	supported at 200 to 28
14° 59' 1/3 ^d	085.655		45° 82.73	(taken backwards) to 28
13° 7' 1/2 ^e	403.005	-.248	45° 392.17	to 29
18° 41' 1/2 ^e	130.755	-.005	45° 123.85	
22° 50' 1/2 ^e	502.60	-.130 -.472	45° 463.00	supported at 200

21 37 1/3 249.40 - .03 44° 231.80 to 26 11916.67
 16° 51 2/3 161.02 - .004 44° 154.08 to 25 11762.59
 12° 6 1/3 185.72 - .004 44° 181.56 to 24. trial line 0.65 too far north 11581.03
 Lev! 169.29 - .004 44° 169.29 114
 to 23 11411.74
 8° 16 1/2 285.865 - .031 42° 282.85 supported at 100
 to 22
 12° 29 3/4 216.82 - .031 42° 211.63
 to 21 supported at 100
 16° 23' 249.525 - .031 42° 239.33
 to 20 10677.93
 21° 19 1/2 312.21 - .033 42° 290.75 supp^d at 200
 19° 48 1/4 565.20 - .433 42° 531.26 to 19 9855.93 from Corce
 14° 29 1/3 512.71 - .451 42° 495.88
 10° 38' 306.405 - .240 42° 399.12 to 18
 6° 7' 130.21 - .004 42° 129.45 to 17
 9° 32' 136.80 - .004 42° 134.89 to 16
 2° 51' 397.70 - .248 42° 396.90 400 - 2.30

8° 30 1/2 271.53 - .032 44° 268.48 to 14
 0° 34' 256.24 - .030 44° 256.19 to 13
 4° 44' 536.57 - .136 44° 534.52 supported at 300
 6° 29 1/3 499.25 - .137 44° 495.84 500 - .75 supported at 200
 to 12
 7° 9 1/4 410.03 - .250 44° 406.53
 8° 39 3/4 306.89 - .106 46° 303.26 to 11
 19° 3 1/2 552.065 - .480 48° 521.28
 20° 56' 406.65 - .243 48° 379.54 to 10 (+.03 to 10)
 26° 38' 304.24 - .033 48° 271.90 supported at 200
 on bearing 236° 15' 40" 500.49 to 10^a
 43° 49 1/3 694.85 - .687 49° on bearing 220° 47 1/2
 50° 57 1/4 113.14 - .003 069.28 taken backwards to old marks on rocks on line
 43° 23' 047.295 034.37
 35° 18' 237.175 - .025 46° 193.53 198.124 2dp⁺ taken backwards
 23° 34' 076.565 70.18 to 6

23

e
16° 54 1/2 495.47 - .246 45° 473.73

3994.4 *from corner*

e
16° 8 1/2 201.005 - .031 44° 193.02

sto 5

e
12° 0 1/3 499.305 - .489 43° 488.17

500 - 0.695 supported at 300 to 4

level 027.05 - 027.05

to tally

e
11° 08 1/2 176.09 - .004 42° 172.75

to 3

e
6° 17 1/2 596.115 - .485 42° 591.95

to 2

e
10° 56 3/4 454.03 - .250 42° 445.46

e
14° 5 2/3 502.69 - .136 - .489 40° 487.33

supported at 300 to 1
e
-15° 9' 298.27 to wad near 287.83 intersection of Res - 2.03

e
10° 27 1/4 263.60 - .032 38° 259.16

e
12° 19 1/4 502.96 - .137 - .489 38° 491.15

supported at 300

e
12° 34' 303.58 - .035 - .106 37° 296.22

" " 200

level 013.91 13.91

to observing sta - folio 1

From Observing Sta near corner

d
15° 0 1/3 318.37 - .06 50° 310.62

d
12° 47 1/4 503.84 - .132 46° 491.14

supported at 300

d
11° 44 1/2 264.73 - .031 47° 259.13

to 1

from intersection to J.R. corner corner tree & peg fd

158° 58' 10" 18.5 T.R. Bdy bears 188° 58' 10"

tree at inter^{sta} 73° 45' Gum
{ 20° 33'
54° 43' }

from intersection with J.R.

d
14° 50 1/2 208.515 - .031 42° 201.50

from tally near ④

~~level 024.26
d
12° 32 1/3 502.15 - .132 46°~~

~~supported at 300 to 5~~

Level 023.03 23.03

d
12° 29 1/3 504.345 - .132 46° 492.21

supported at 300 to 5

3985 post ^u 33° 37' Gum { 16° 30'
142 45 Gum { 21° 0'
5° 53'
53° 55' }

3996.5 pipe

24 From (12)

7° 15 1/2 d 499.99 - 134 46 495.47 sup^{td} at 300

(500-01)

5° 23 d 537.12 - 135 44 534.53 to (13)

At 8010 18° 56' Pepper mid 41.45
139° 25' " 452



From 19

19° 27 e 563.64 - 133 48 531.28 supported at 200

20° 40 1/2 e 310.82 - 48° 290.76 no sag to 20

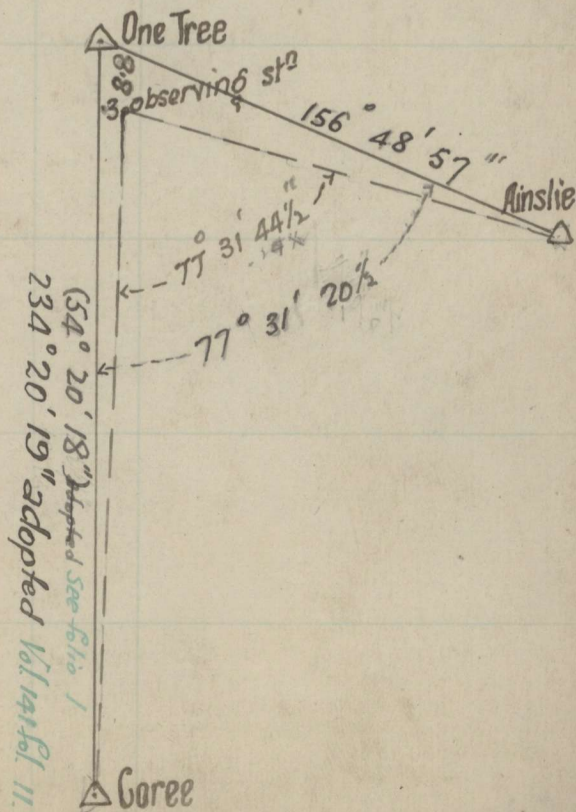
15° 27 1/2 e 248.38 - .01 48 239.34 supported at 100

to 21

25 ^{st² near} Angle observed at One Tree between Ainslie and Coree Trig

On Ainslie	On Coree	Angle by subtraction	Angle by division
0° 0' 0"	77° 31' 47"	77° 31' 47"	77° 31' 47"
155	03 35	77 31 48	77 31 47
232	35 19	77 31 44	77 31 45
310	07 02	77 31 43	77 31 45
27	38 42	77 31 40	77 31 44
105	10 23	77 31 42	77 31 41
182	42 07	77 31 44	77 31 44
260	13 55	77 31 48	77 31 44

One Tree to Ainslie 156° 48' 57"
Ainslie - Coree (angle) 77° 31' 21"
One Tree Δ - Coree Δ = 234° 20' 18" bearing on Strom meridian



P.L.S. 11.7.1910